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1. INTRODUCTION

This document provides the procedures for performing the final radiological survey of Building T011, formerly known as the "Radiation Instrument Calibration Laboratory". The scope of this survey includes a 100% direct qualitative scan for alpha and beta-gamma contamination followed by a 11% cumulative count survey of interior surfaces of "affected" areas in the north section of the building where handling of radioactive materials occurred. The remaining parts of the north section of the building are classified as "unaffected" areas and will be surveyed by a 10% qualitative scan, followed by a 2%/5% cumulative count survey. The southern portion of the building was an unrelated facility, not used in any way for radiological work, and is therefore excluded from consideration in this survey.

This survey will ensure that all areas of Building T011 will meet all NRC, DOE and State of California criteria for release of the facility for unrestricted use. The sampling inspection by variables method will be applied to the data obtained in this survey procedure. The in-house computer code "CumPlot" will be used for data analysis and presentation of survey report results.

This is a final survey procedure for a clean facility. Any areas that exceed limits of this procedure shall be decontaminated per a separate special procedure and an additional survey performed to document those areas as meeting all DOE, NRC and State of California criteria for release of a facility for unrestricted use.

1.1 Building History

The north section of the building was used for calibration and repair of radiation instrumentation over a time period from 1984 to 1996. This activity involved the regular use of radioactive sources for calibration, most of which were sealed. Work activities included the repair of radiation detection equipment which may have been contaminated when used on various decommissioning and decontamination (D&D) projects. The south section of the building was used by the Property Inventory and Control department as a general storage warehouse and has no history of storage or handling of radioactive materials.

A spot survey of several rooms in the north section was performed in March 1996 during transfer of counting equipment from the building to T100. Although the results of this spot survey indicated no observable radionuclide contamination, it was deemed prudent to perform a release radiological survey of the north section to verify that no residual contamination exists from unsuspected causes. The primary nuclides of interest during this survey will be Cs-137, Co-60, Sr-90, Eu-152, Eu-154, thorium, and uranium.

2. SAMPLING PLAN OVERVIEW

The final radiological survey of Building T011 requires a series of specific steps in the sample lots to be surveyed. Distinguishable properties for selecting the sampling lots are rooms in Building T011 where there was known, or suspected, use or presence of radioactive materials. The areas included in the sampling lots are listed below (see Figure 1 for location of rooms in T011):

Sample Lot 1 (Affected Areas): Rooms 100, 102, 104, 105, 106, 108, 111, and adjacent

hallways.

Sample Lot 2 (Unaffected Areas): Rooms 101, 103, 118, 120, 121, 122, 124, and adjacent

hallways.

If contamination or high ambient radiation above 25% of release guidelines is found in any areas from Sample Lot 2, those areas will be re-classified as "affected", and surveyed at a 100% level. If necessary, a procedure will be written to decontaminate any rooms with contamination exceeding allowable limits, and document the findings. And such rooms will be re-surveyed to the limits prescribed in this procedure.

2.1.1 Walls, Floors and Ceiling

For affected areas, direct qualitative scan of 100% of the floor, walls, and ceiling shall be conducted. Following the scan, a uniform 3-m x 3-m grid shall be laid out on the floor, ceiling and walls, starting in one room at the northwest corner. One 1-m x 1-m area within each 3-m x 3-m grid shall be selected for a cumulative count survey. A minimum of 30 data points shall be selected in each sample lot. For surfaces having areas less than 1-m x 1-m, a minimum area of 1-m x 1-m shall be surveyed by combining the other adjacent remnant areas.

For affected areas, additional surveying will be conducted underneath selected floor tiles in each room or area. The floor tiles in T011 are older type 9-in. x 9-in. tiles which have been shown to contain sufficient levels of asbestos to be classified as Asbestos Containing Material (ACM). Typically, the floor mastic used to attached these tiles is also classified as ACM. The floor tiles will be randomly selected, or chosen from areas where tiles have already been removed or are only loosely adhered to the sub-floor due to years of exposure and moisture leakage. Removal of tiles which remain firmly adhered to the sub-floor will be conducted as needed by trained asbestos abatement personnel. It is probable that areas where the tiles have already been removed, or are only loosely adhered, are areas where potential contamination would be more likely to exist.

For unaffected areas, a direct qualitative scan of 10% of the floors, walls, and ceilings shall be conducted. Areas of particular concern should include floor baseboards, window sills, areas behind file cabinets or other furniture, door thresholds, and any other areas where contamination

would be likely to have accumulated over time. Following the surface scan, a uniform 3-m x 3-m grid shall be laid out on the floors, wall, and ceilings, as described above. Randomly select one 1-m x 1-m grid floor and wall grid within every two 3-m x 3-m grids (approximately 5%), and one 1-m x 1-m ceiling grid within every five 3-m x 3-m (approximately 2%), for cumulative count survey. A minimum of one data point for every 50 m² shall be obtained.

2.1.2 Structural Surfaces

Structural surfaces consist of beams, pipes, conduits, and other surfaces that are not amenable to large surface measurements. Twenty percent of the structural surfaces shall be surveyed for affected areas, and 10% for unaffected areas. The selection of surfaces to survey should be biased toward those expected to have the highest contamination levels (e.g. ledges, tops of conduit, etc.).

2.1.3 Concrete Pads

Concrete pads shall be surveyed as a floor area in the same manner as indicated in Section 2.1.1.

2.1.4 Sink Traps

Sink traps located in the unaffected areas shall be sampled for potential contamination. This sampling shall include a 100% scan on the outside of the trap (including gamma radiation), a smear survey inside the trap, and if possible, sludge collection for gamma spectroscopy analyses from the inside bottom of the trap.

2.1.5 Roofs

Heating and air conditioning systems for the north section of T011 are located on the roof of the building. Return air ducts in both affected and unaffected areas of T011 will be surveyed for possible contamination. If no contamination is found, the roof of the facility will be deemed clean. If contamination is found, this procedure will be red-lined indicating additional survey steps required. If contamination is found above release limits, the registers will be decontaminated and resurveyed per Section 1.

2.2 Instrument Calibrations and Checks

Measurements of the average and maximum alpha surface activities shall be made with alpha scintillation detectors, sensitive only to alpha particles with energies exceeding about 1.5 MeV. The detectors shall be calibrated with a Th-230 alpha source standard. Measurements of the average and maximum beta surface activities shall be made with a thin-window pancake Geiger-Mueller tube. The detectors shall be calibrated with a Tc-99 beta source standard.

All portable survey instruments shall be serviced and calibrated on a quarterly basis. Daily checks and calibrations shall be performed on all instrumentation (when used) to determine

Mean Standard Radionuclide Value^a Deviation^b (pCi/g) (pCi/g) Naturally occurring 238_[J] 0.64 0.24 235[] 0.02 0.03 ²³²Th 0.97 0.36 ^{40}K 15.3 5.6 Man-made ¹³⁷Cs 0.0^{c} 0.0 134Cs 0.0 0.0 ⁶⁰Co 0.00.0

Table 1. Summary of Gamma Spectrometry Data for All 199 T009 Drain Line Soil Samples

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3.3 COMPARISON WITH BACKGROUND RADIONUCLIDE ACTIVITY LEVELS AT THE SSFL

Because radionuclide activity, including the fission product ¹³⁷Cs, was observed in the inactive SGR hold-up tank sludge sample, it is instructive to examine the radionuclide data in Table 1 to determine if the measured activities are consistent with naturally occurring radioactivity levels at the SSFL. This will verify that no unobserved leaks occurred in the drain line system during its operation that may have contaminated the surrounding soil.

Background radionuclide activity is present at the SSFL, and elsewhere, as a result of several naturally occurring radionuclides and also from the man-made nuclide ¹³⁷Cs from radioactive fallout during the period of atmospheric nuclear weapons testing. Background values for radionuclide activity at the SSFL were independently measured as part of an Area IV survey by Groundwater Resources Consultants (GRC), Inc. between July and October 1988 (Ref. 6). Measured background values for ²³⁸U, ²³⁵U, ²³²Th, ¹³⁷Cs, and ⁴⁰K from the survey are summarized in Table 2. The activity values in Table 2 are an average of data from three representative soil samples taken during the GRC survey.

^aMean value of 199 soil data values (Appendix A).

bStandard deviation (10) of distribution.

^cMean value includes two data points with values of 0.15 and 0.18 pCi/g, which were above the cutoff limit for the measuring equipment (see text).

Comparing the data in Tables 1 and 2 indicates that in each case the radionuclide values measured in the Building T009 soil are consistent although somewhat lower than the corresponding GRC values. The zero average ¹³⁷Cs value for the T009 soil samples in Table 1 may be attributed to that fact that the soil was taken from around the buried drain lines, and thus was underground and largely unaffected from any fallout. The measured ratio of ²³⁵U to ²³⁸U in the drain line soil is also consistent, within uncertainties, with the GRC measured ratio, and the expected naturally occurring activity ratio of 0.045 (Ref. 7) for these two isotopes.

Thus, the data show no increased residual activity either from the ¹³⁷Cs fission product, from the ²³⁸U and ²³⁵U fuel element isotopes, or from ²³²Th, which could have potentially contaminated the soil in the vicinity of the drain lines.

Although the comparison of the data in Tables 1 and 2 indicates that there is no residual radionuclide activity from ¹³⁷Cs, ²³⁸U, or ²³⁵U in the Building T009 drain line soil, the data do indicate some small systematic differences in the T009 data and the corresponding background data determined by GRC. Figures 2, 3, and 4 show the ratio of ²³⁸U, ²³²Th, and ²³⁵U with respect to the naturally occurring ⁴⁰K data, for each of the 199 soil samples plotted against the cumulative gaussian probability. The value of this type of graphical display is that it permits the identification of individual data points significantly outside the range expected for the distribution. For a perfectly "normal" (gaussian) distribution, the data values would fall on a straight line, with the mean value

Table 2. Summary of Background Soil Radionuclide Activity at the SSFL

Isotope	Mean Value ^a (pCi/g)	Standard Deviation ^b (pCig)
Naturally occurring		
$^{238}\mathrm{U}$	1.1	0.3
235 _U	0.04	0.02
²³² Th	1.7	0.3
$^{40}\mathrm{K}$	22	1
<u>Man-made</u>		
¹³⁷ Cs	0.07	0.05

Note: Data from Groundwater Resources Consultants (GRC) Report 8640M-77 (Ref. 6)

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^aAverage of data from three representative soil samples.

^bStandard deviation (10) of distribution.

Figure 2. Measured ²³⁸U/⁴⁰K Ratio in T009 Drain Line Soil

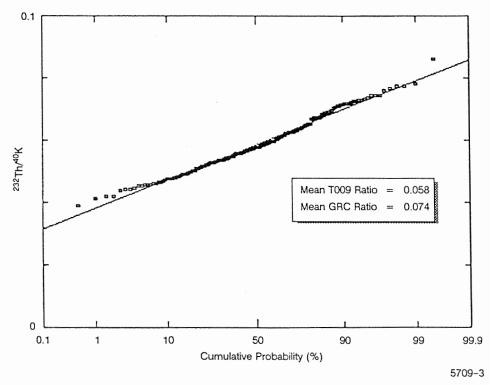


Figure 3. Measured ²³²Th/⁴⁰K Ratio in T009 Drain Line Soil

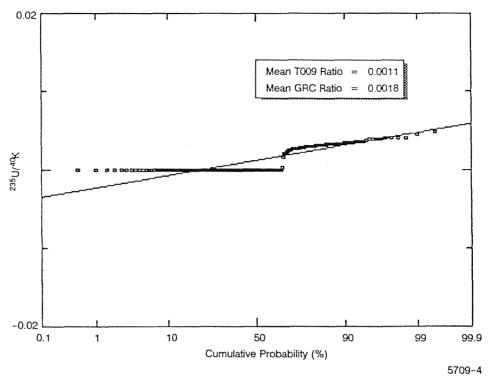


Figure 4. Measured ²³⁵U/⁴⁰K Ratio in T009 Drain Line Soil

occurring at the 50% point on the probability axis. For comparison, the mean ratio values for the T009 data and the GRC data are also indicated inside each figure.

Figures 2 and 3 show distributions which are closely gaussian, with no outliers. The distribution in Figure 4, for ²³⁵U, also shows no outliers but it is slightly skewed due to a large number of "zero" measurements. The mean isotope ratios obtained from the Building T009 data, although being similar to the corresponding GRC values, are nonetheless consistently lower. These comparisons, therefore, suggest that there are some small energy-dependent sensitivity and/or calibration differences between the Canberra instrument used at the SSFL and the analysis system used by GRC Inc. These differences, however, have no effect on the overall conclusions reached from the data.

\$5.6% \$2.5 (14.4-14.8) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (14.4) \$1.5 (

4.0 CONCLUSIONS

In accordance with the recommendations of the Building T009 radiological survey, the inactive SGR hold-up tank and associated drain line system were removed under Health Physics supervision for disposal at an authorized site. As part of this work, extensive soil samples were taken for subsequent gamma spectrometric analysis and the results were compared with background radionuclide activity levels at the SSFL. These analyses are reported here, and the following conclusions are drawn.

4.1 SPECIFIC CONCLUSIONS

- 1. No residual levels of man-made radionuclides were observed in the T009 drain line soil.
- 2. Measured naturally occurring radionuclide activity in the Building T009 drain line soil was comparable to (although slightly lower than) normal background levels measured independently in nearby soils at the SSFL.
- 3. The slightly lower T009 soil activity results compared to normal background levels are attributed to small variations in the sensitivity and/or calibration of the SSFL analysis system.

4.2 OVERALL CONCLUSIONS

- 1. Based on the results of the analyses reported here, the Building T009 drain line soil is free of any residual radioactive contamination.
- 2. Based on the results of the 1988 radiological survey of Building T009, the OMR side (interior western side) and the outside northwestern areas surveyed are acceptably free of residual radioactive contamination.
- 3. The interior western side and the exterior northwestern side are suitable for release for use without radiological restrictions.

5.0 REFERENCES

- 1. Chapman, J. A., "Radiological Survey of Building T009," GEN-ZR-0014, Rocket-dyne Division, Energy Technology Engineering Center, Rockwell International, August 26, 1988.
- 2. Badger, F. H., and Tuttle, R. J., "Radiological Survey Plan for SSFL," 154SRR000001, Rocketdyne Division, Rockwell International, September 25, 1985.
- 3. Klein, A., "Building T009 Drain System Removal," N001TI000329, Rocketdyne Division, Rockwell International, August 22, 1990.
- 4. Parker, D. C., "SGR Liquid Drain Line System Removal, Building T009," 195DWP000001, Rocketdyne Division, Rockwell International, October 10, 1989.
- 5. Chapman, J. A., "Radiological Survey of the Source and Special Nuclear Material Storage Vault Bldg T64," GEN–ZR–0005, Energy Technology Engineering Center, Rockwell International, August 19, 1988.
- 6. "Investigation of Naturally Occurring Radionuclides in Rock, Soils and Groundwater Santa Susana Field Laboratory, Ventura County, California," 8640M–77, Groundwater Resources Consultants, Inc., June 1, 1990.
- 7. Lederer, C. M. and Shirley, V. S. (Eds.), "Table of Isotopes," 7th ed., John Wiley, New York, 1978.

APPENDIX A

DERIVED ALPHA, BETA, AND RADIONUCLIDE DATA FROM BUILDING T009 DRAIN LINE SOIL

During removal of the SGR hold-up tank and associated drain line system from Building T009, 199 two-pound samples were collected from the soil surrounding the drain lines. In each case, samples ranging in mass from ~700 to 900 g were analyzed using a Canberra system as described in Ref. 2. Following analysis, the results were input to the MCASOIL spreadsheet, which calculated derived quantities for total alpha and total beta, and derived activities for selected man-made and naturally occurring radionuclides. A zero value in the data tables indicates that no photopeaks were detected above the detection limit of the Canberra multichannel analyzer. For ¹³⁷Cs, this detection limit was ~0.1 to 0.2 pCi/g for the counting times used for the analyses.

Table A-1. Gamma Spectrometry Data from Drain Line Soil Samples (Sheet 1 of 6)

					(1)	neet 1 or	-07					
	39	40	41	42	43	44	45	46	47	48	49	50
1	BUILDING T009 DRAIN LINE	SOIL SAMP	LES									
2	(Samples Analyzed: 1/11/90	TO 1/18/90)										
3	Excel File:	009SOIL.XI	_S									
4												
5		•		***********	plcocurie	s per gram c	of each radio	nuclide				
6					186 keV	185.6 keV						
7			U-238	Th-232	U-235	U-235	K-40	Cs-137	Cs-134	Co-60	Derived Alpha	Derived Beta
8					(from	(from					pCi/g	pCi/g
9					Ra-226)	U-238)						
10 11	Sample	Mass	c32*1e6/	c33*1e6/	c34*1e6/	c41*.045	c35*1e6/	c36*1e6/	c37*1e6/	c38*1e6/	8*c41±6*c421	
12	Description	(grams)	c2	c2	c2	011 1010	¢2	c2	c2	c2		c43+sum(c44:48)
13	***************************************	(3,)			······································							
14	SOIL 1	708.2	0.74	1.11	0.04	0.03	16.50	0.00	0.00	0,00	12.88	25.58
15	SOIL 2	584.9	0,63	1.15	0.00	0.03	16.76	0.00	0.00	0.00	11.89	25.14
16	SOIL 3	494.8	0.73	1.13	0.00	0.03	19.48	0.00	0.00	0.00	12.59	28.39
17	SOIL 4	630.4	0.65	1.09	0.00	0.03	17.39	0.00	0.00	0.00	11.75	25.69
18	SOIL 4 DUPLICATE	698.0	0.67	0.79	0.04	0.03	13.85	0.00	0.00	0.00	10.41	21.24
19	SOIL 5	659.2	0.67	1.05	0.00	0.03	18.31	0.00	0.00	0.00	11.62	26.53
20	SOIL 6	649.4	0.84	1,06	0.05	0.04	17.01	0.00	0.00	0.00	13.48	26.56
21	SOIL 7	628.7	0.87	1.09	0.06	0.04	17.57	0.00	0.00	0.00	13.93	27.44
	SOIL 8	659.1	0.62	1.19	0.00	0.03	16,34	0.00	0.00	0.00	12.11	24.85
23	SOIL 9	639.4	0.69	1.07	0.00	0.03	16,50	0.00	0.00	0.00	11.92	24.93
24	SOIL 10	670.1	0.73	0.74	0.04	0.03	17.68	0.00	0.00	0.00	10.60	25.24
	SOIL 11	776.4	0.53	0.74	0.00	0.02	14.19	0.00	0.00	0.00	8.64	20.32
	SOIL 12	699.7	0.71	0.95	0.00	0.03	16,10	0.00	0.00	0.00	11.34	24.17
	SOIL 12 DUPLICATE	716.1	0.55	0.87	0.00	0.02	15,08	0.00	0.00	0.00	9.65	21.91
	SOIL 13	717.0	0.74	0.98	0.05	0.03	15,41	0.00	0.00	0.00	12.15	24.00
	SOIL 14	724.7	0.59	0.89	0.00	0.03	16.69	0.00	0.00	0.00	10.08	23.84
	SOIL 15	739.9	0,55	0.97	0.00	0.02	14.48	0.00	0.00	0.00	10.28	21.73
{	SOIL 16	627.4	0.97	1.10	0.00	0.04	16.77	0.00	0.00	0.00	14.32	27.00
	SOIL 17	558.4	1.01	1.01	0.07	0.05	17.71	0.00	0.00	0.00	14.57	28.09
	SOIL 18	665.7	0.62	1.07	0.00	0.03	16.51	0.00	0.00	0.00	11.37	24.53
	SOIL 19	730.3	0.58	0.75	0.00	0.03	13.39	0.00	0.00	0.00	9.18	19.92
	SOIL 30	741.5	0.82	0,82	0.05	0.04	15.16	0.00	0.00	0,00	11.79	23.57
36	SOIL 31	785.2	0.62	0.81	0.00	0.03	13.89	0.00	0.00	0,00	9.85	20.91

Table A-1. Gamma Spectrometry Data from Drain Line Soil Samples (Sheet 2 of 6)

								·					
	T	39	40	41	42	43	44	45	46	47	48	49	50
37	SOIL 3	32	782.7	0.73	0.81	0.06	0.03	15.14	0.00	0.00	0.00	11.15	23.05
38	SOIL 3	33	785.8	0.57	0.80	0.00	0.03	13.81	0.00	0.00	0.00	9.35	20.45
39	SOIL :	34	726.3	0.48	0.69	0.00	0.02	14.68	0.00	0.00	0.00	7.95	20.32
40	SOIL 3	35	724.2	0.58	0.79	0.00	0.03	14.64	0.00	0.00	0.00	9.36	21.30
41		36	691.3	0.49	0.79	0.00	0.02	14.14	0.00	0.00	0.00	8.62	20.23
42	SOIL	37	772.7	0.54	0.71	0,00	0.02	13.33	0.00	0.00	0.00	8.56	19.42
43	SOIL 3	38	725.2	0.56	0.89	0.00	0.03	14.97	0.00	0.00	0.00	9.77	21.88
44	SOIL 3	39	728.9	0.64	0.70	0.00	0.03	14.97	0.00	0.00	0.00	9.29	21.62
45	SOIL 4	40	738.9	0.70	0.77	0.05	0.03	14.50	0.00	0.00	0.00	10.65	22.06
46	SOIL 4	41	713.5	0.65	0.63	0.00	0.03	14.98	0.00	0.00	0.00	8.99	21.43
47	SOIL 5	52	819.6	0.71	1.04	0.04	0.03	14.97	0.00	0.00	0.00	12.18	23.57
48	SOIL 5	53	704.9	0.59	1.16	0.00	0.03	16.87	0.00	0.00	0.00	11.70	25.09
49	SOIL 5	54	761.1	0.58	0.86	0.00	0.03	15.59	0.00	0.00	0.00	9.85	22.58
50	SOIL 5	55	661.3	0.66	1.01	0.00	0.03	15.71	0.00	0.00	0.00	11.34	23.74
51	SOIL 5	56	776.0	0.68	1.09	0.04	0.03	15.05	0.00	0.00	0.00	12.24	23.66
52	SOIL 5	57	818.2	0.92	1.11	0.04	0.04	15.28	0.00	0.00	0.00	14.25	25.41
53	SOIL 5	58	677.2	0.76	1.06	0.04	0.03	15.80	0.00	0.00	0.00	12.67	24.76
54	SOIL 5	58 DUPLICATE	693.2	0.58	1.03	0.00	0.03	13.80	0.00	0.00	0.00	10.83	21.44
55	SOIL 5	59A	640.8	0.90	1,15	0.06	0.04	15.79	0.00	0.00	0.00	14.52	26.07
56	SOIL 6	60A	808.6	0.60	0.99	0.04	0.03	15.09	0.00	0.00	0.00	11,00	22.83
57	SOIL 6	62	705.4	0.55	0.84	0.00	0.02	18.43	0.00	0.00	0.00	9.44	25.11
58]SOIL 6	53	739.0	0.67	1.01	0.00	0.03	14.29	0.00	0.00	0.00	11.42	22.38
59	SOIL 6	54	690.5	0.73	0.79	0.05	0.03	15.79	0.00	0.00	0.00	10.89	23.54
60	SOIL 6	65	752.3	0.67	0.87	0.04	0.03	17.03	0.00	0.00	0.00	10.83	24.70
61	SOIL 7	70	613.0	0.66	1.09	0.00	0.03	17.37	0.00	0.00	0.00	11.80	25.71
62	SOIL 7	71	678.5	0.81	0.87	0.05	0.04	16.89	0.00	0.00	0.00	12.05	25.47
63	SOIL 7	72	665.2	0.70	1.00	0.00	0.03	17.03	0.00	0.00	0.00	11.60	25.26
64	SOIL 7	73	650.7	0.68	0.94	0.00	0.03	16.81	0.00	0.00	0.00	11.07	24.67
65	SOIL 7	74	774.0	0.52	0.82	0.00	0.02	15.02	0.00	0.00	0.00	9.12	21.47
66	SOIL 7	75	710.0	0.58	0.96	0.00	0.03	17.55	0.00	0.00	0.00	10.44	24.93
67	SOIL 7	76	679.5	0.92	1.18	0.06	0,04	13.73	0.00	0.00	0.00	14.85	24.24
68	SOIL 7	77	717.9	0.71	1.13	0.05	0.03	15.17	0.00	0.00	0.00	12.82	24.19
69	SOIL 7	78	612.4	0.80	1.09	0.06	0.04	17.41	0.00	0.00	0.00	13.37	26.85
70	SOIL 7	79	636.1	0.88	1.03	0.05	0.04	17.70	0.00	0.00	0.00	13.64	27.38
71	SOIL 8		771.2	0.57	0.73	0.00	0.03	15.14	0.00	0.00	0.00	8.93	21.50
72	SOIL B	30 DUPLICATE	641.3	0.74	1.18	0.06	0.03	18.46	0.00	0.00	0.00	13.35	27.85

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81	30	40	41	42	43	44	45	46	47	48	49	50
811.9 0.54 82 811.9 0.54 85 800.7 0.69 86 804.3 0.58 87 815.7 0.63 88 823.2 0.55 89 772.0 0.56 90 778.8 0.82 102 772.4 0.48 103 772.4 0.48 104 772.4 0.48 105 603.9 0.60 104 775.0 0.62 105 624.8 0.80 115 624.8 0.80 115 624.8 0.80 115 624.8 0.80 115 624.8 0.80 115 624.8 0.83 115 624.8 0.83 115 623.2 0.54 115 623.2 0.54 116 623.2 0.54 117 77.9 0.54 118 774.7 0.54 119 623.2 0.76 119 672.7 0.82 119 672.7 0.82	ä	792.7	0.61	0.76	0.0	0.03	14.42	0.0	0.00	00:00	9.46	21.17
83 789.6 0.61 865 866 866 867 968 868 869.7 0.63 868 869.3 0.58 868 869.3 0.58 869 869.3 0.58 869 869 869 869 869 869 869 869 869 86		811.9	0.54	0.68	0.00	0.05	14.62	0.00	0.00	0.00	8.43	20.63
84 774.1 0.57 85 804.3 0.69 86 804.3 0.69 87 803.2 0.63 89 792.0 0.56 89 772.8 0.82 90 772.4 0.48 102 772.4 0.48 103 772.4 0.48 104 772.4 0.49 105 624.8 0.80 1121 765.9 0.54 1122 774.0 0.63 1124 774.0 0.63 1126 624.8 0.80 1129 774.0 0.63 1120 623.2 0.76 1121 774.0 0.63 1122 776.0 0.63 1124 774.0 0.63 1125 698.9 0.51 1126 623.2 0.76 1127 774.0 0.63 1128 774.0 0.63 1129 774.0 0.63 1120 623.2 0.76 1121 774.7 0.82 1122 174.7 0.64 1123 774.0 0.63 1124 774.7 0.64 1125 691.5 0.68 1126 623.2 0.76 1127 0.82 1128 0.87 1129 0.67 1120 0.68		789.6	0.61	0.68	0.0	0.03	14.55	0.00	0.0	0.0	8,95	20.95
855 866 867 867 868 868 869 87 864.3 865.8 869 87 8823.2 855.8 89 87 8823.2 855.8 89 89 772.8 89 8023.2 855.8 89 8023.2 805.8 808 808 808 808 808 808 808 808 808 8		774.1	0.57	0.81	0.0	0.03	13.97	0.00	0.00	0.00	9.41	20.65
866 804.3 0.58 804.3 0.58 804.3 0.58 804.3 0.58 805 805 805 805 805 805 805 805 805 8		800.7	69.0	99.0	0.05	0.03	14.58	0.00	00'0	0.00	9.81	21.59
823.2 0.63 89 823.2 0.55 89 792.0 0.56 90 778.8 0.82 100 772.4 0.48 101 772.4 0.48 102 772.4 0.48 103 772.4 0.48 104 772.4 0.48 105 603.9 0.60 106 603.9 0.60 107 775.0 0.62 108 624.8 0.80 109 624.8 0.80 110 775.0 0.63 110 774.0 0.63 110 623.2 0.76 110 623.2 0.54 110 774.0 0.63 110 623.2 0.76 110 623.2 0.76 110 623.2 0.76 110 774.0 0.63 110 623.2 0.76 110 62 63 110 62 63 110 62 63 110 62 63 110 63 1		804.3	0.58	0.80	0.0	0.03	14,32	0.00	0.0	0.00	9.45	21.03
823.2 0.55 89 792.0 0.56 90 778.8 0.82 91 772.4 0.48 100 603.9 0.60 101 772.4 0.48 102 772.4 0.48 103 772.4 0.48 104 772.4 0.48 105 623.9 0.60 106 624.8 0.80 107 776.0 0.62 108 624.8 0.80 117 776.9 0.54 117 774.0 0.63 118 623.2 0.76 118 623.2 0.76 119 623.2 0.76 119 623.2 0.76 119 623.2 0.76 119 623.2 0.76 119 672.7 0.82 119 672.7 0.82		815.7	0.63	0.84	0.0	0.03	14.91	0.0	0.0	0.0	10.14	22.12
792.0 0.56 90 778.8 0.82 91 772.4 0.48 100 603.9 0.60 101 772.4 0.48 102 772.4 0.48 103 776.0 0.62 104 725.2 0.49 105 624.8 0.80 106 624.8 0.80 1174 775.9 0.59 1175 774.0 0.63 1176 698.9 0.51 1176 672.7 0.82 1179 672.7 0.82		823.2	0.55	0.73	8.0	0.02	14.22	0.00	0.00	0.0	8.77	20.46
90 778.8 0.82 91 772.4 0.48 92 772.4 0.48 100 772.4 0.48 101 772.4 0.48 102 772.4 0.45 103 777.0 0.62 104 776.0 0.62 105 776.0 0.62 106 624.8 0.80 120 765.9 0.54 121 765.9 0.54 122 774.0 0.63 124 774.7 0.54 125 779.9 0.51 126 623.2 0.76 127 623.2 0.76 128 623.2 0.76 129 623.2 0.76 120 623.2 0.76 121 672.7 0.82 122 774.5 0.82 123 775.9 0.51 124 774.7 0.63 125 150 623.2 0.76 126 152 0.51 127 151 0.82 128 152 0.68 129 152 0.69 120 152 0.51 120 152 0.69 120 152 0.51 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69 120 152 0.69		792.0	0.56	0.92	0.0	0.03	15,36	0.00	00'0	0.00	9:95	22.39
91 772.4 0.48 99 772.4 0.48 100 603.9 0.60 101 772.4 0.48 102 776.0 0.62 103 776.0 0.62 104 786.2 0.62 105 776.0 0.62 106 624.8 0.80 120 765.9 0.54 121 797.2 0.59 122 774.0 0.63 123 774.7 0.54 126 698.9 0.51 150 623.2 0.76 151 672.7 0.82 152 691.5 0.82 153 623.2 0.76 154 774.5 0.68 155 691.5 0.68 156 691.5 0.68 156 601.5 0.68 157 601.5 0.68 158 705.2 0.61 159 601.5 0.68 150 601.5 0.68 150 601.5 0.68 150 601.5 0.68 150 601.5 0.69 150 601.5		778.8	0.82	0.77	90.0	0.04	14.04	0.00	0.00	0.0	11.60	22.32
99 772.4 0.48 603.9 0.60 100 603.9 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.		782.6	0.41	0.81	8.0	0.02	15.08	0.00	0.00	8.0	8.11	20.71
100 603.9 0.60 101 717.4 0.45 102 736.9 0.60 103 766.2 0.62 104 725.2 0.49 105 624.8 0.80 1106 624.8 0.80 1107 775.9 0.54 1108 774.0 0.63 1109 774.0 0.63 1109 623.2 0.76 1109 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100 623.2 0.76 1100		772.4	0.48	0.72	0.0	0.05	15.75	0.00	0.00	0.0	8.15	21.52
101 717.4 0.45 102 736.9 0.53 104 766.2 0.62 105 766.2 0.62 106 624.8 0.80 106 624.8 0.80 120 725.2 0.49 121 725.9 0.80 122 736.6 0.54 123 774.7 0.54 124 774.7 0.54 125 774.0 0.63 150 698.9 0.51 151 672.7 0.82 152 691.5 0.82 153 691.5 0.82 154 724.5 0.68 155 705.2 0.51 156 705.2 0.51 156 705.2 0.51 156 705.2 0.51 156 705.2 0.51 157 668 774.5 0.68 156 705.2 0.51 157 705.2 0.51 158 70		603.9	0,60	0.97	0.0	0,03	15.89	0.00	0.00	0.00	10.60	23.38
102 736.9 0.53 103 776.0 0.62 104 766.2 0.62 105 776.0 0.62 106 624.8 0.80 120 816.1 0.49 121 765.9 0.54 122 736.6 0.59 123 774.7 0.54 126 774.7 0.54 127 774.7 0.54 150 698.9 0.51 151 672.7 0.82 152 691.5 0.82 153 691.5 0.87 154 724.5 0.68 155 691.5 0.87 154 724.5 0.68 155 705.2 0.51 156 724.5 0.68 157 681.5 0.68 156 705.2 0.51 157 681.5 0.68 158 705.2 0.51 159 681.5 0.68 150 681.5 0.68 150 681.5 0.68 150 681.5 0.68 150 681.5 0.61 150 681.5		717.4	0.45	0.73	0.0	0.02	13.43	0.00	0.00	0.00	7.97	19.06
103 776.0 0.62 104 766.2 0.62 105 766.2 0.62 106 624.8 0.80 120 816.1 0.49 121 765.9 0.54 122 797.2 0.59 123 774.7 0.54 126 774.7 0.54 150 623.2 0.76 151 623.2 0.76 152 631.5 0.82 153 672.7 0.82 154 724.5 0.68 155 707.8 0.87 156 691.5 0.68 156 691.5 0.68 156 774.5 0.68 156 672.7 0.82 156 672.7 0.68 156 705.2 0.68 156 705.2 0.51 157 705.2 0.51 158 705.2 0.51 159 605.1 605.1 150 605.2 605.1 150 605.2 605.1 150 605.2 605.1 150 605.2 605.1 150 605.2<		736.9	0.53	0.90	0.00	0.02	14.33	0.00	0.00	0.0	9.64	21.13
104 766.2 0.62 105 725.2 0.49 106 624.8 0.80 120 816.1 0.49 121 765.9 0.54 122 736.6 0.58 123 774.7 0.54 126 774.7 0.54 150 698.9 0.51 151 623.2 0.76 152 691.5 0.82 153 672.7 0.82 154 724.5 0.68 155 707.8 0.87 156 691.5 0.68 156 691.5 0.68 156 774.5 0.68 157 705.2 0.51 156 705.2 0.51 157 705.2 0.51 158 705.2 0.51 159 705.2 0.51 150 60.47		776.0	0.62	0.55	0.0	0.03	11,32	0.00	0.00	0.00	8.26	17.26
105 725.2 0.49 106 624.8 0.80 120 816.1 0.49 121 765.9 0.54 122 797.2 0.59 123 774.7 0.58 124 774.7 0.54 125 774.7 0.63 150 698.9 0.51 151 623.2 0.76 152 691.5 0.82 153 691.5 0.82 154 724.5 0.68 155 707.8 0.87 156 705.2 0.61 156 691.5 0.68 157 0.68 0.76 158 705.2 0.51 150 0.51 0.68 150 0.51 0.68 150 0.51 0.68 150 0.51 0.68 150 0.51 0.67 150 0.51 0.67 150 0.51 0.67 150 0.69 0.74		766.2	0.62	0.76	9.0	0.03	13.90	0.0	0.00	0.00	9.80	20.85
126 624.8 0.80 127 765.9 0.54 128 797.2 0.59 129 774.7 0.58 126 774.7 0.54 126 774.0 0.63 126 698.9 0.51 150 623.2 0.76 151 623.2 0.76 152 691.5 0.82 153 691.5 0.82 154 724.5 0.68 155 691.5 0.82 156 891.5 0.82 157 0.82 158 0.72 159 0.51 150 0.82 150 0.82 151 0.82 152 0.82 153 0.82 154 707.8 0.87 155 0.68		725.2	0.49	0.78	0.0	0.02	13.24	0.00	0.00	0.0	8.58	19.31
120 816.1 0.49 121 765.9 0.54 122 736.6 0.59 123 774.7 0.54 125 774.0 0.63 126 777.9 0.51 150 698.9 0.51 151 672.7 0.82 153 691.5 0.82 154 724.5 0.68 155 705.2 0.51 156 816.8 0.47		624.8	0.80	0.81	90.0	9.0	15.67	0.00	0.0	0.0	11.71	24.01
121 765.9 0.54 122 797.2 0.59 123 736.6 0.58 124 774.7 0.64 125 774.0 0.63 126 774.0 0.63 150 698.9 0.51 151 623.2 0.76 152 691.5 0.82 153 691.5 0.82 154 724.5 0.68 156 705.2 0.51 160 816.8 0.47		816.1	0.49	0.77	0.00	0.02	14.81	0.00	0.0	0.0	8.49	20.81
122 797.2 0.59 123 736.6 0.58 124 774.7 0.54 125 774.0 0.63 126 774.0 0.63 150 698.9 0.51 151 623.2 0.76 152 623.2 0.76 153 623.2 0.76 154 707.8 0.82 155 707.8 0.87 156 724.5 0.68 150 816.8 0.47		765.9	0.54	0.81	0.0	0.02	14.47	0.00	0.00	0.00	9.19	20.99
123 736.6 0.58 124 774.7 0.54 125 774.0 0.63 126 774.0 0.63 150 698.9 0.51 151 623.2 0.76 152 672.7 0.82 153 691.5 0.82 154 707.8 0.87 155 707.8 0.68 156 705.2 0.51 160 816.8 0.47	•	797.2	0.59	0.92	0.0	0.03	13,55	0.0	0.00	0.00	10.21	20.77
124 774.7 0.54 125 774.0 0.63 126 779.9 0.51 150 698.9 0.52 151 623.2 0.76 152 691.5 0.82 153 691.5 0.82 154 707.8 0.87 155 705.2 0.51 156 816.8 0.47		736.6	0.58	0.96	0.03	0.03	13.94	0.00	0.00	0.00	10.65	21.43
125 774.0 0.63 126 779.9 0.51 150 698.9 0.52 151 623.2 0.76 152 672.7 0.82 153 691.5 0.82 154 724.5 0.68 155 705.2 0.51 160 816.8 0.47		774.7	0,54	0.81	0.0	0.02	11.40	0.15	0.00	0.0	9.20	18.07
126 779.9 0.51 150 698.9 0.52 151 623.2 0.76 152 672.7 0.82 153 691.5 0.82 154 707.8 0.87 155 705.2 0.51 160 816.8 0.47		774.0	0.63	0.85	0.00	0.03	13.58	0.00	0.00	0.00	10.10	20.76
150 698.9 0.52 151 623.2 0.76 152 672.7 0.82 153 691.5 0.82 154 707.8 0.87 155 705.2 0.51 160 816.8 0.47		279.9	0.51	0.79	0.00	0.02	10.28	0.00	0.00	0.00	8.85	16.54
151 623.2 0.76 152 672.7 0.82 153 691.5 0.82 154 707.8 0.87 155 705.2 0.51 160 816.8 0.47		698.9	0.52	96.0	0.0	0.05	15.73	0.00	0.00	0.00	9.90	22.69
152 672.7 0.82 153 691.5 0.82 154 707.8 0.87 155 705.2 0.51 160 816.8 0.47		623.2	0.76	1.10	0.05	0.03	16.34	0.00	0.00	0.00	13.02	25.52
153 691.5 0.82 154 707.8 0.87 155 724.5 0.68 156 816.8 0.47	- •	672.7	0.82	1.13	0.00	0.04	14.48	0.00	0.00	0.00	13.37	23.98
154 707.8 0.87 155 724.5 0.68 156 705.2 0.51 160 816.8 0.47		691.5	0.82	1.07	0.05	0.04	14.30	0.00	0.00	00.00	13.33	23.73
155 724.5 0.68 156 705.2 0.51 160 816.8 0.47	•	707.8	0.87	1.08	90.0	0.04	14.30	0.00	0.00	0.00	13.88	24.13
156 705.2 0.51 160 816.8 0.47	- •	724.5	0.68	0.82	0.0	0.03	13.71	0.00	0.0	0.00	10.62	21.25
160 816.8 0.47	. •	705.2	0.51	0.88	0.00	0.02	12.32	0.0	0.0	0.0	9.39	20.00
	-	816.8	0.47	0.70	0.0	0.02	11.59	0.00	0.00	0.00	8.02	17.20
161 /38.8 0.34		758.8	0.54	1.11	0.00	0.02	15.75	0.0	0.00	0.0	11.00	25.40
739.7 0.53		739.7	0.53	0.85	0.03	0.02	13.38	0.00	0.0	0.00	9.53	20.03

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Table A-1. Gamma Spectrometry Data from Drain Line Soil Samples (Sheet 4 of 6)

							-	Control of the last of the las			
39	40	41	42	43	44	45	46	47	48	49	50
109 SOIL 1000	800.7	0.54	0,62	0.04	0.02	10.49	0.00	0.00	0.00	8.26	16.35
110 SOIL 1001	756.6	0.67	0.68	0.00	0.03	14.14	0.0	0.00	0.0	9.49	20.95
111 SOIL 1002	807.5	0.52	0.65	0.0	0.02	14.90	0.0	0.00	0.0	8.12	20.69
112 SOIL G1	667.4	0.59	0.88	0.00	0.03	15.93	0.00	0.00	0.00	10.03	23.04
113 SOIL G2	6.089	0.61	0.86	0.00	0.03	15.78	0.0	0.00	0.00	10.04	22:90
114 SOIL G3	631.7	0.62	0.73	0.0	0.03	15.96	0.0	0.00	0.00	9.38	22.65
115 SOIL G5	573.6	0.95	0.97	90.0	0.04	18.05	0.00	0.00	0.00	13.88	27.94
116 SOIL G6	747.8	0.47	0.62	0.00	0.02	10.01	0.18	0.00	0.00	7.49	15.52
117 SOIL G7	692.2	0.61	0.80	0.00	0.03	15.44	0.00	0.0	0.0	9.71	22.35
118 SOIL G9	700.1	0,58	0.73	0.00	0.03	14.99	0.00	0.00	0.0	9.02	21.42
119 SOIL G10	677.7	0.56	0.94	0.0	0.03	15.69	0.00	0.0	0.0	10.06	22.79
120 SOIL G11	717.2	0.68	0.75	0.04	0.03	15.36	0.0	0.00	8.0	10.22	22.63
121 SOIL G13	678.9	0.65	98.0	0,03	0.03	16,35	0.00	0.00	8.0	10.54	23.82
122 SOIL 914	670.2	0.73	0.75	0.0	0.03	14.01	0.00	0.0	0.0	10.30	21.39
123 SOIL 015	689.4	0.55	0.73	0.00	0.02	14.14	0.00	0.00	0.00	8.78	20.38
124 SOIL G30	759.5	0.67	0.95	0.00	0.03	13,22	0.00	0.00	0.00	11.00	21.03
125 SOIL G31	644,4	0.83	1.36	0.05	0.04	19,15	0.00	0.00	0.00	15.14	29.79
126 SOIL 032	729.1	0.56	0.95	0.00	0.03	17.57	0.00	0.00	00:00	10.16	24.75
127 SOIL 933	603.6	0.81	1.13	0.00	0.04	17.56	0.00	0.00	0.00	13.26	26.97
128 SOIL 034	719.9	0.80	1.8	0.04	0.04	13,13	0.00	0.0	0.00	12.71	22.15
129 SOIL 035	686.2	0.78	1.10	0.05	0.03	15.94	0.00	0.00	0.00	13.19	25.25
130 SOIL 036	2.099	0.67	0.85	0.00	0.03	13.95	0.00	0.00	0.00	10.44	21.38
131 SOIL G37	9'969	0.72	0.90	0.05	0.03	15.16	0.00	8.0	0.00	11.53	23.32
132 SOIL 639	653,6	0.58	1.14	0.00	0.03	14.76	0.00	0.00	0.00	11.48	22.82
133 SOIL G40	750.8	0.58	0.99	0.00	0.03	14.00	0.00	0.00	0.00	10.58	21.47
134 SOIL G41	738.0	0.80	0.94	0.05	0.04	16.59	0.00	0.00	0.00	12.43	25.42
135 SOIL G42	643.8	0.56	0.95	0.0	0.03	17.72	0.0	0.00	0.00	10.21	24.93
136 SOIL G42	831,9	0.64	0.77	0.02	0.03	15.14	0.00	0.00	0.00	68'6	22.17
137 SOIL 643	0.797	0.71	06.0	0.00	0.03	15.12	0.00	0.00	0.00	11.07	23.00
138 SOIL G44	727.0	0,83	0.97	90.0	0.04	15.65	0.00	0.00	0.0	12.87	24.78
139 SOIL G44 DUPLICATE	768.2	0.62	0.86	0.0	0.03	15.31	0.00	0.00	0.00	10,11	22,49
140 SOIL G45	748.3	0,61	0.78	0.00	0.03	13.66	0.00	0.00	0.00	9.54	20.45
141 SOIL G45 DUPLICATE	814.3	0.72	0.86	0.00	0.03	15.43	0.00	0.00	0.0	10.91	23.21
142 SOIL G46	681.8	0.59	0.92	0.05	0.03	14.15	0.00	0.0	0.00	10,60	21.61
143 SOIL G46 DUPLICATE	806.2	0.74	0.82	0.05	0.03	14.66	0.00	0.00	0.0	11.15	22.59
144 SOIL G47	667.2	0.89	0.82	90.0	0.0 40.0	17.80	0.0	0.0	0.0 0.0	12.44	89.92

· 建物等的原理。

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	39	40	41	42	43	44	45	46	47	48	49	50
9	G47 DUPLICATE	606.4	0.60	0,83	0.00	0.03	17.34	0.0	0.00	0.00	9.77	
G48	8	768.1	0.68	0.72	0.05	0.03	15,57	0.00	0.0	0.00	10.07	
G49	0	644.3	0.57	0.91	0.00	0.03	16,12	0.00	0.00	0.00	10.03	
85	0	601.5	0.80	99.	90:0	9.0	18.09	0.00	0.00	0.00	13.20	
149 SOIL GE	G50 (60000 SECOND	601.5	0.72	1.01	9.0	0.03	16.30	0.0	0.0	0.00	12.11	
921	_	646.6	0.60	1.08	0.0	0.03	18,11	0.00	0.00	0.00	11.32	
G 52	2	734.3	0.55	0.97	0.00	0.02	13,99	0.0	0.00	0.00	10.16	
SOIL G53	8	711.4	99'0	0.68	0.00	0.03	14.33	0.0	0.00	0.00	9.39	
99	0	676.6	0.49	0.91	0.00	0.02	15.98	0.0	0.00	0.00	9,34	
9	-	705.5	0.50	0.81	0.00	0.02	13,45	0.0	0.00	0.00	8.90	
SOIL G62	2	701.0	0.58	0.74	9.0	0.03	14.50	0.0	0.00	0.00	9.30	
963	en en	754.2	0.53	69'0	0.00	0.02	14.55	0.00	0.00	0.00	8.40	
157 SOIL G64	₹	6.999	0.52	0.65	0.00	0.02	14.63	0.00	0.00	0.00	8.06	
158 SOIL G65	Ω	0'689	0.43	0,65	0.0	0.02	14,36	0.0	0.0	0.00	7.30	
159 SOIL GE	S	710.0	0.63	0.68	0.00	0.03	13.63	0.0	0.00	0.00	9.11	
160 SOIL 970	C	790.2	0.50	0.78	0.00	0.02	13.51	00'0	0.00	0.00	8.72	
SOIL G71	_	795.4	0.65	0.81	0.00	0.03	15,43	00'0	0.00	0.00	10,04	
162 SOIL G72		777.1	0.59	0.76	0.00	0.03	15.15	0.00	0.00	0.00	9.28	
163 SOIL G73	3	784.8	0.72	0.79	0.05	0.03	13.85	0.00	0.00	0.0	10.80	
164 SOIL G74	77*	798.6	0.64	0.87	0.04	0.03	13.03	0.00	0.00	0.0	10.69	
165 SOIL G75	10	7777.5	0,59	0.68	0.0	0.03	15.38	0.00	0.00	0.00	8.76	
166 SOIL G78		761.1	0.56	0.80	0.00	0.03	12.49	0.00	0.0	0.00	9.25	
G79	£	6'69'	0.50	0.75	0.00	0.02	13.00	0.00	0.00	0.00	8.48	
SOIL G80		792.3	0.51	0.75	0.00	0.02	12.77	0.00	0.0	0.00	8.58	
	G80 DUPLICATE	789.6	0.64	0.78	9.04	0.03	14.79	0.00	0.00	0.00	10.10	
170 SOIL G81		738.8	0.59	0.77	0.00	0.03	14.86	0.00	0.00	0.00	9.30	
SOIL 682	61	785.2	0.60	0.72	0.04	0,03	14.49	0.00	0.00	0.00	9.43	
SOIL G83	~	767.5	0.70	0.79	0.04	0.03	14.74	0.00	0.00	0.00	10.61	
173 SOIL G84		801.8	0.65	0.86	0.00	0.03	13.99	0.00	0.00	00'0	10.35	
G85	10	818.7	0.74	0.62	0.04	0.03	15.10	9.00	0.00	0.00	9.93	
SOIL G87		756.2	0.73	0.71	0.0	0.03	14.78	0.00	0.00	0.00	10.04	
176 SOIL G88	~	785.2	0.74	0.72	0.05	0.03	11.55	0.00	0.00	0.00	10.61	
	G88 DUPLICATE	805.3	0.64	0.68	0.0	0.03	13.95	0.00	0.00	0.00	9.55	
SOIL G89	•	1.608	0.60	0.73	0.00	0.03	14.75	0.0	0.00	0.00	9.14	
179 SOIL G90		768.6	0.53	0.69	0.00	0.02	13.94	0.00	0.00	0.00	8.41	
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24.28 27.42 27.42 27.42 27.42 27.42 27.42 27.42 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27.66 27